

STATIC EQUIVALENT LOADING: 949 STYLE BACKSTOP

CEILING SUSPENDED, FORWARD FOLD, FRONT BRACED

INTRODUCTION

The following pages show the estimated reaction forces of a backstop- up to the point of structure that is custom designed for each individual project. Custom-designed structure may add overall weight to the assembly, but normally distributes these reaction forces to the building attachment points.

Final reaction magnitude and locations cannot be determined until the backstop is engineered, but this document is meant to serve as a worst-case guide for your project. The reaction forces are based on the weight of the backstop (including the heaviest backboard, height adjuster, etc) and a 0.7 Seismic Factor.

CLICK ON YOUR ATTACHMENT HEIGHT BELOW:

[18' Attachment Height](#)

[23' Attachment Height](#)

[28' Attachment Height](#)

[19' Attachment Height](#)

[24' Attachment Height](#)

[29' Attachment Height](#)

[20' Attachment Height](#)

[25' Attachment Height](#)

[30' Attachment Height](#)

[21' Attachment Height](#)

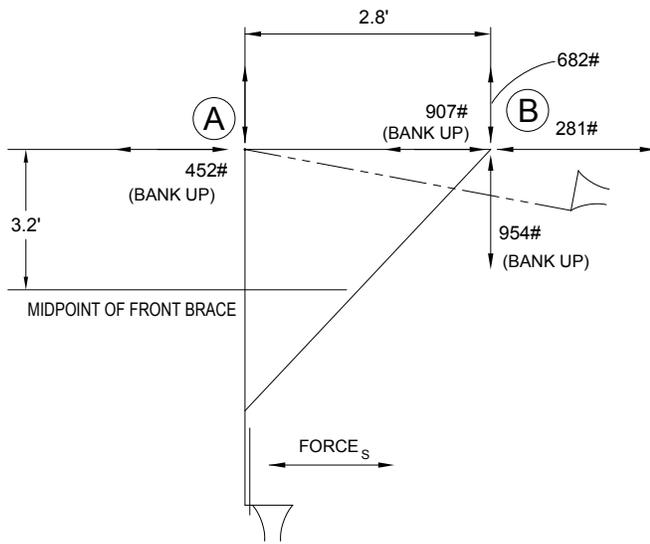
[26' Attachment Height](#)

[31' Attachment Height](#)

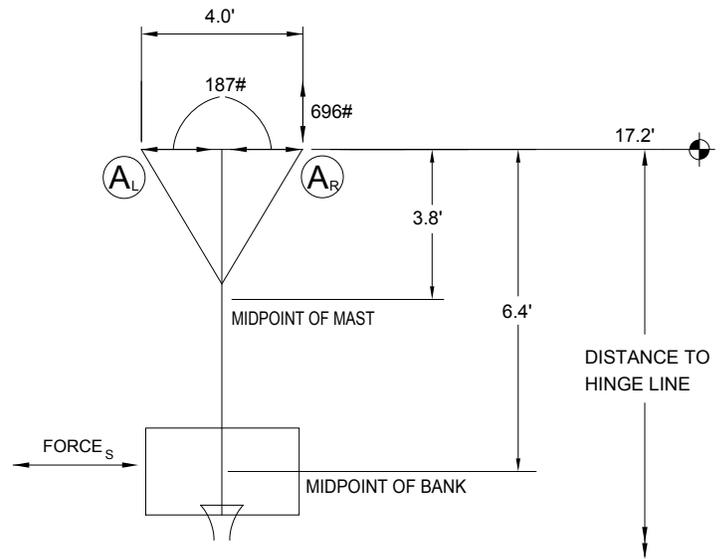
[22' Attachment Height](#)

[27' Attachment Height](#)

[32' Attachment Height](#)



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	534 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		487 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$	
WEIGHT LOAD AT POINT "B" =		47 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	1189 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	22 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	50 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	212 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	570 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 1808 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN	R_{VER}^A	VERTICAL REACTIONS AT POINT A:	$696 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$
	R_{HOR}^A	HORIZONTAL REACTION AT POINT A:	$187 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN	R_{VER}^B	VERTICAL REACTION AT POINT B:	$682 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$
	R_{HOR}^B	HORIZONTAL REACTION AT POINT B:	$281 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $907 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{A-BU}	VERTICAL REACTION AT POINT A:	$-186 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$
	R_{HOR}^{A-BU}	HORIZONTAL REACTION AT POINT A: FROM SEISMIC PARALLEL TO BANK	$452 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{B-BU}	VERTICAL REACTION AT POINT B:	$954 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$
	R_{HOR}^{B-BU}	HORIZONTAL REACTION AT POINT B:	$907 \text{ lbs} = \text{HOIST CABLE TENSION}$



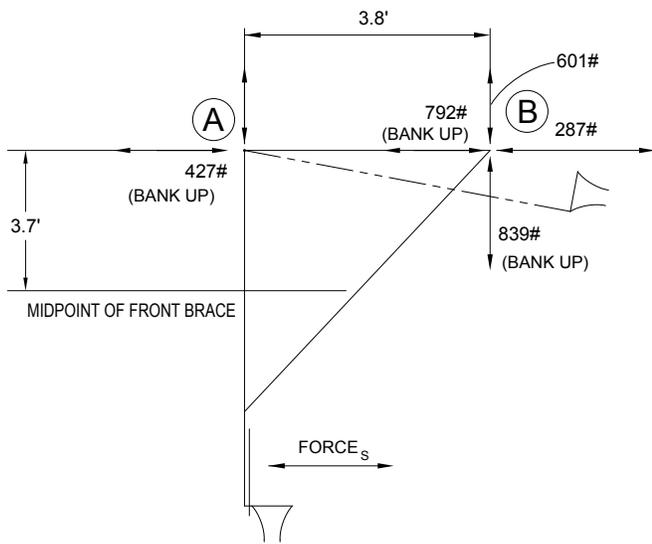
REVISION	DATE	porter No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		DATE
5/9/2011		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style backstop
18' Attachment Height

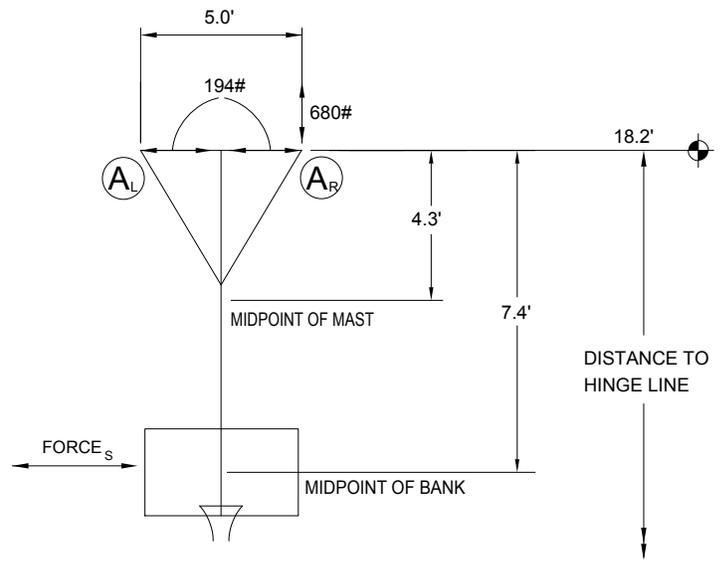
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 553 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.)

WEIGHT LOAD AT POINT "A" = 506 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = 47 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	1373 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	22 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	57 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	231 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	703 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 2134 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $680 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $194 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $601 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $287 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $792 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $-119 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $427 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$ FROM SEISMIC PARALLEL TO BANK

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $839 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $792 \text{ lbs} = \text{HOIST CABLE TENSION}$



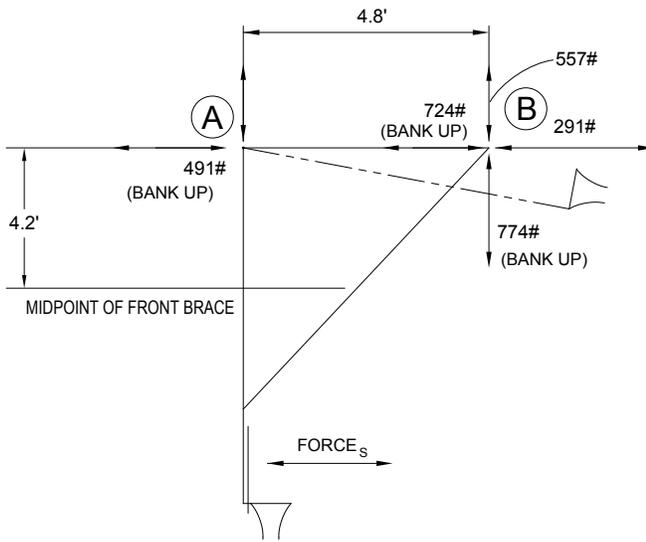
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
19' Attachment Height

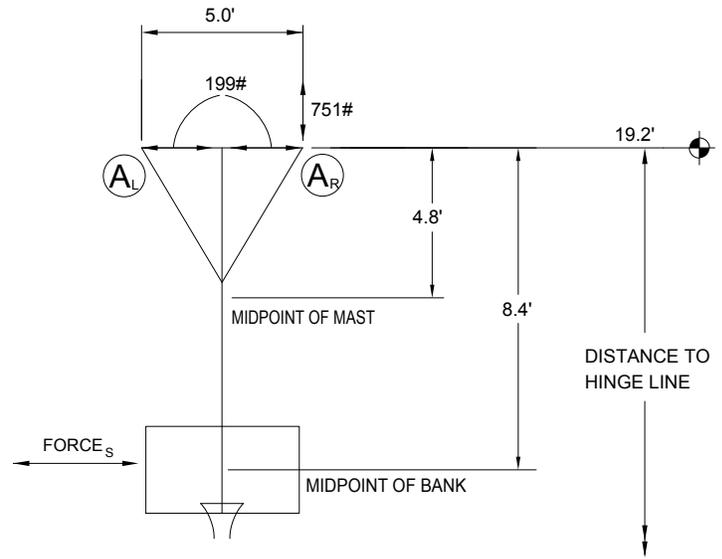
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	trmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 569 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MOST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = 519 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = 50 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB) 264 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF BANK (DB) = 1558 ft.lbs SEISMIC MOMENT (MB) (FT.LBS.)

WEIGHT OF FRONT BRACE (WFB) 28 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF FRONT BRACE (DFB) = 83 ft.lbs SEISMIC MOMENT (MFB) (FT.LBS.)

WEIGHT OF MAST (WM) 241 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF MAST (DM) = 816 ft.lbs SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 2457 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: 751 lbs = $\frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_2\text{A)}_R}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: 199 lbs = $\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: 557 lbs = $\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: 291 lbs = $\frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: 724 lbs = $\frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: -78 lbs = $\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: 491 lbs = $\pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_2\text{TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: 774 lbs = HOIST CABLE TENSION + $\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: 724 lbs = HOIST CABLE TENSION



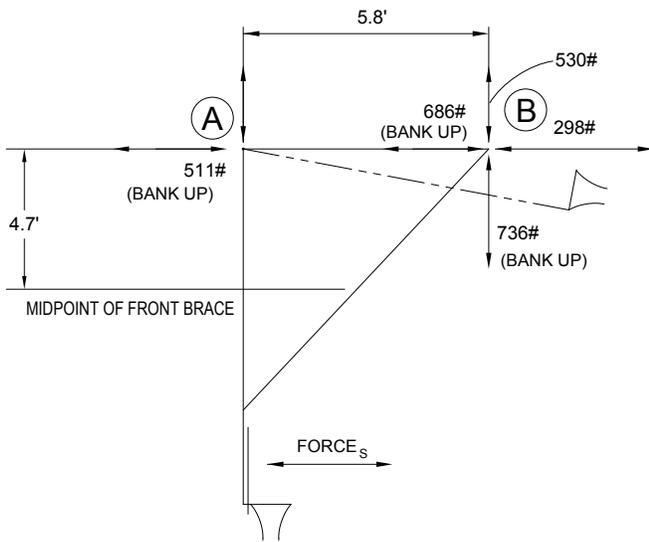
REVISION	DATE	PORTER No. C11
A	6/7/95	
B	7/31/95	CUSTOMER No. 3064
C	6/1/99	
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
20' Attachment Height

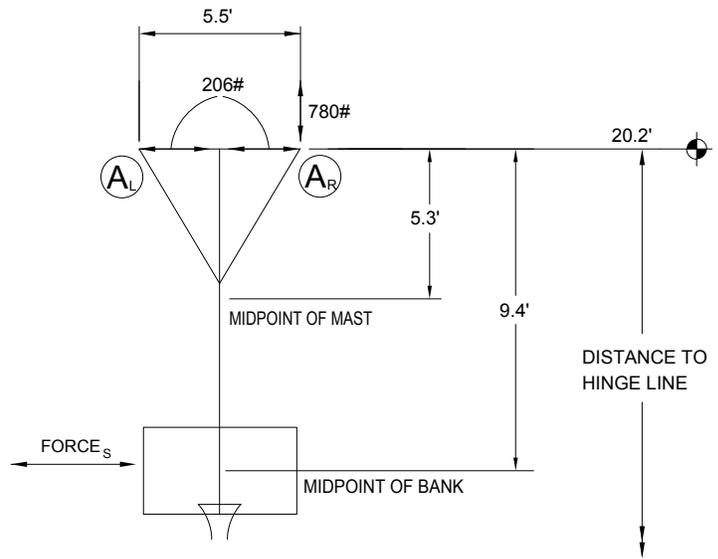
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY tmathis
 CHECKED BY GS
 PAGE No.



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	588 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		538 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK	
WEIGHT LOAD AT POINT "B" =		50 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	1743 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	28 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	92 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	260 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	974 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 2809 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $780 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $206 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $530 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $298 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $686 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $-49 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: FROM SEISMIC PARALLEL TO BANK $511 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $736 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $686 \text{ lbs} = \text{HOIST CABLE TENSION}$



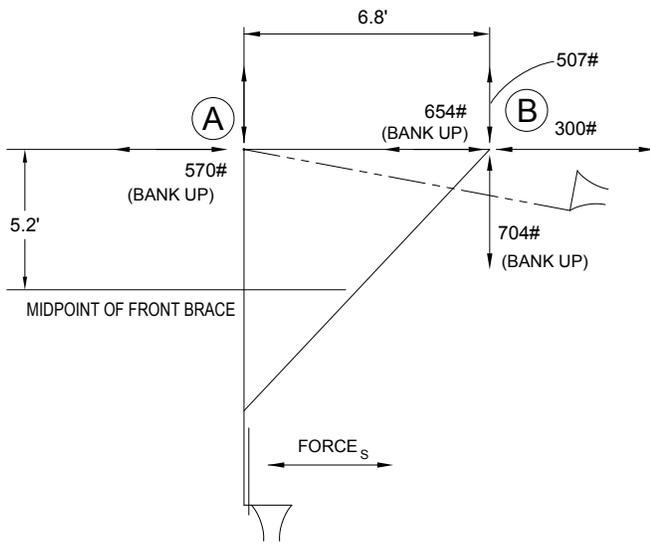
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		
5/9/2011		

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
21' Attachment Height

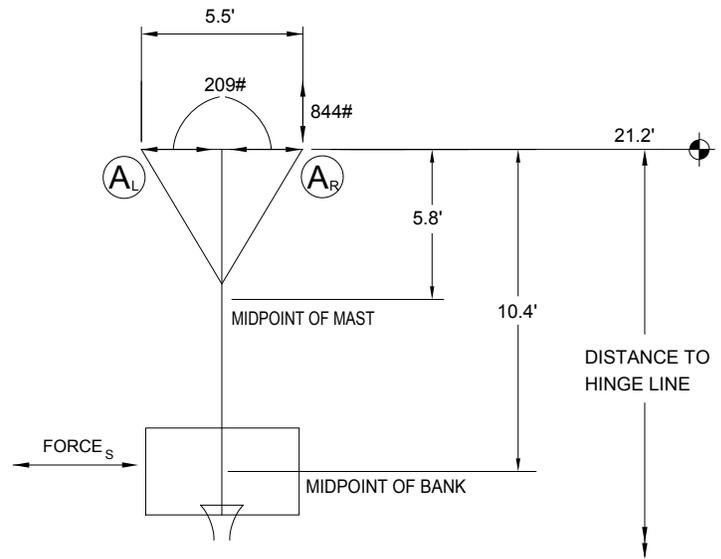
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	598 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		548 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$	
WEIGHT LOAD AT POINT "B" =		50 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	1928 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	28 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	102 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	270 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	1103 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)
WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD			=	3133 ft.lbs	SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN	R_{VER}^A	VERTICAL REACTIONS AT POINT A:	$844 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{-A}_R\text{)}}_R$
	R_{HOR}^A	HORIZONTAL REACTION AT POINT A:	$209 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN	R_{VER}^B	VERTICAL REACTION AT POINT B:	$507 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$
	R_{HOR}^B	HORIZONTAL REACTION AT POINT B:	$300 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $654 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{A-BU}	VERTICAL REACTION AT POINT A:	$-28 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$
	R_{HOR}^{A-BU}	HORIZONTAL REACTION AT POINT A: FROM SEISMIC PARALLEL TO BANK	$570 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{B-BU}	VERTICAL REACTION AT POINT B:	$704 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$
	R_{HOR}^{B-BU}	HORIZONTAL REACTION AT POINT B:	$654 \text{ lbs} = \text{HOIST CABLE TENSION}$



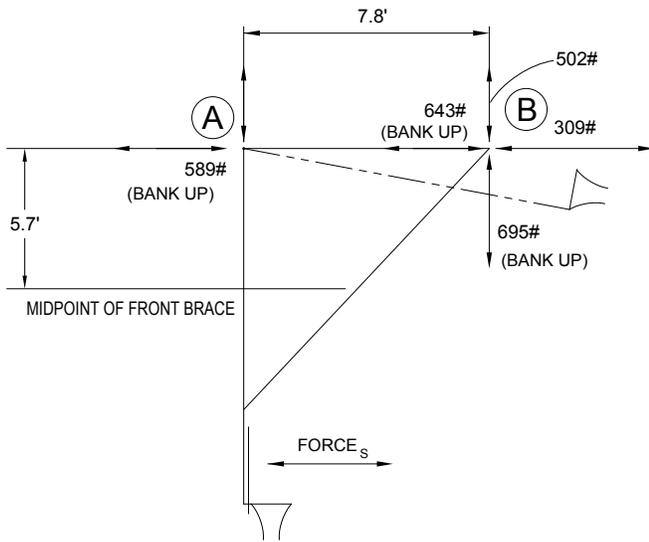
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		
5/9/2011		

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
22' Attachment Height

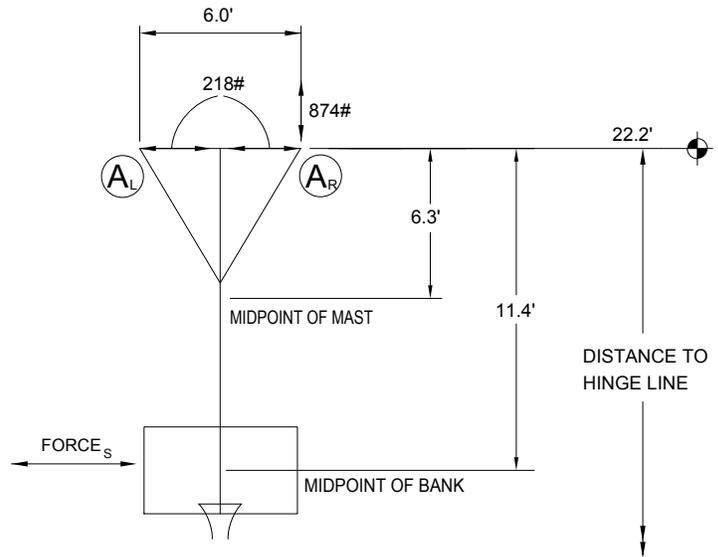
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	623 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		570 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK	
WEIGHT LOAD AT POINT "B" =		53 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	2113 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	33 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	132 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	290 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	1287 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 3531 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $874 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $218 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $502 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $309 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $643 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $-10 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $589 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $695 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $643 \text{ lbs} = \text{HOIST CABLE TENSION}$



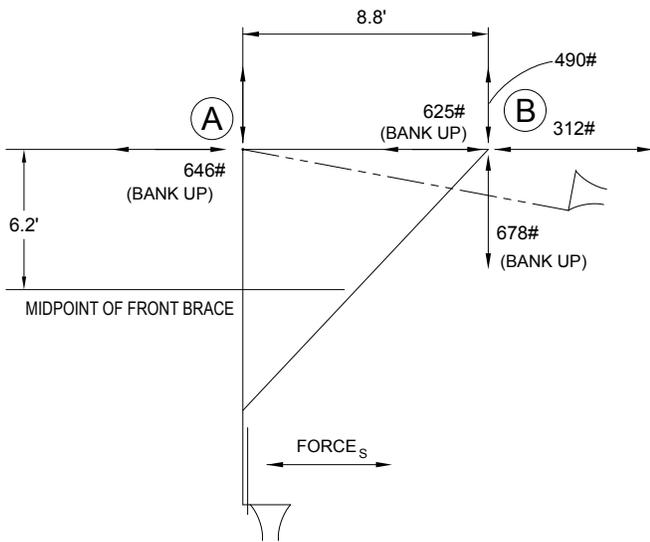
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
23' Attachment Height

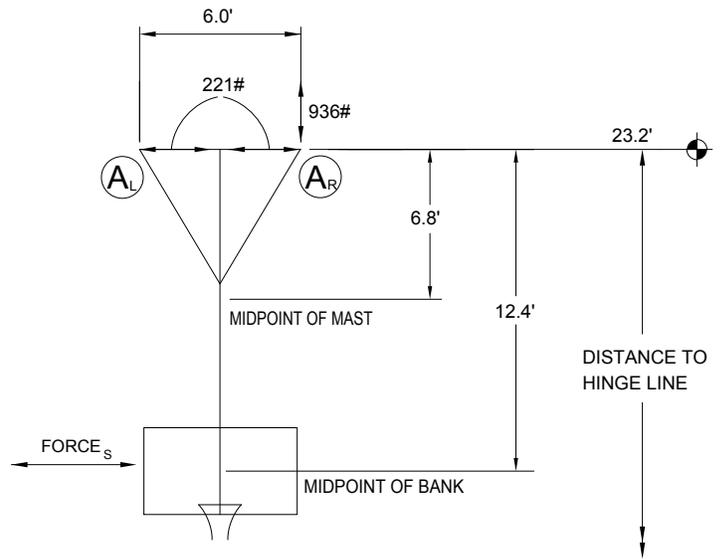
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	632 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		$580 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$	
WEIGHT LOAD AT POINT "B" =		$53 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	2297 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	33 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	144 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	299 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	1433 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 3874 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN	R_{VER}^A	VERTICAL REACTIONS AT POINT A:	$936 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS } (A_L A_R)_R}$
	R_{HOR}^A	HORIZONTAL REACTION AT POINT A:	$221 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN	R_{VER}^B	VERTICAL REACTION AT POINT B:	$490 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS } (A-B)}$
	R_{HOR}^B	HORIZONTAL REACTION AT POINT B:	$312 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $625 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{A-BU}	VERTICAL REACTION AT POINT A:	$3 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$
	R_{HOR}^{A-BU}	HORIZONTAL REACTION AT POINT A: FROM SEISMIC PARALLEL TO BANK	$646 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{B-BU}	VERTICAL REACTION AT POINT B:	$678 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$
	R_{HOR}^{B-BU}	HORIZONTAL REACTION AT POINT B:	$625 \text{ lbs} = \text{HOIST CABLE TENSION}$



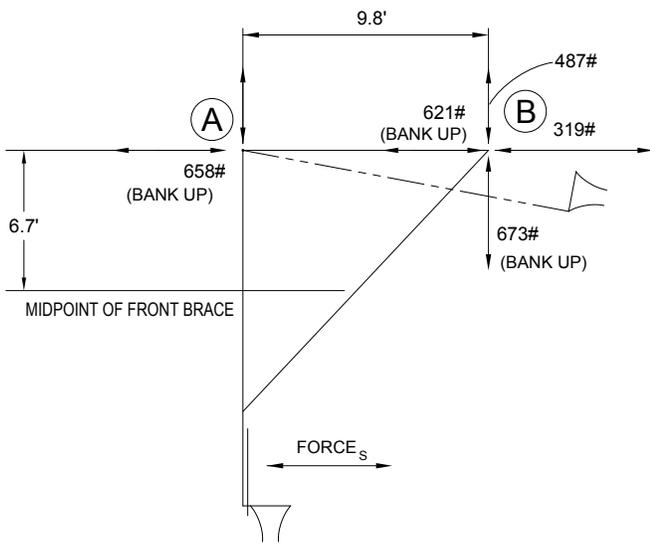
REVISION	DATE	PORTER No. C11
A	6/7/95	
B	7/31/95	CUSTOMER No. 3064
C	6/1/99	
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
24' Attachment Height

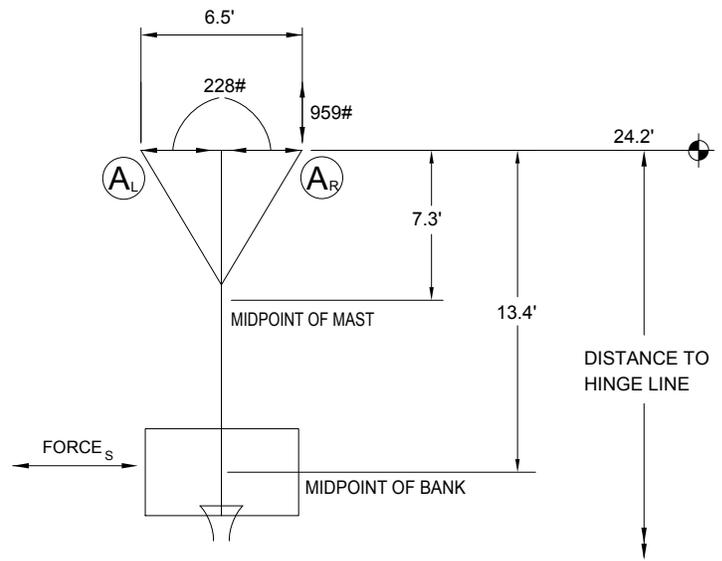
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	trmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 653 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = 600 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = 53 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	2482 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	33 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	155 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	320 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	1643 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 4280 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $959 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $228 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $487 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $319 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $621 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $16 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $658 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $673 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $621 \text{ lbs} = \text{HOIST CABLE TENSION}$



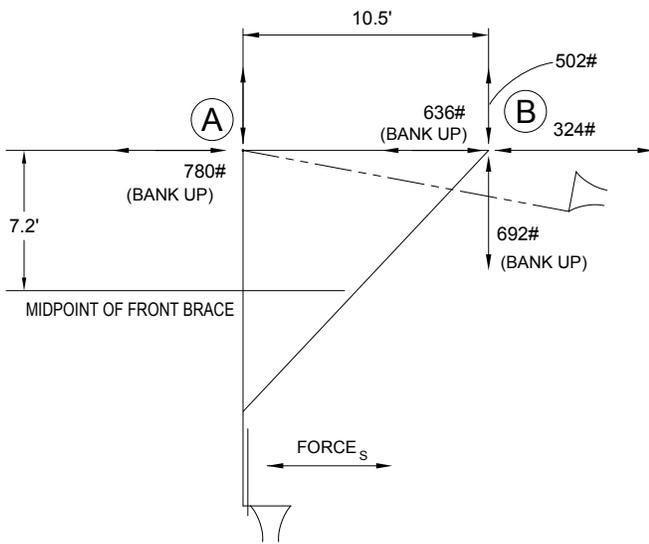
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
25' Attachment Height

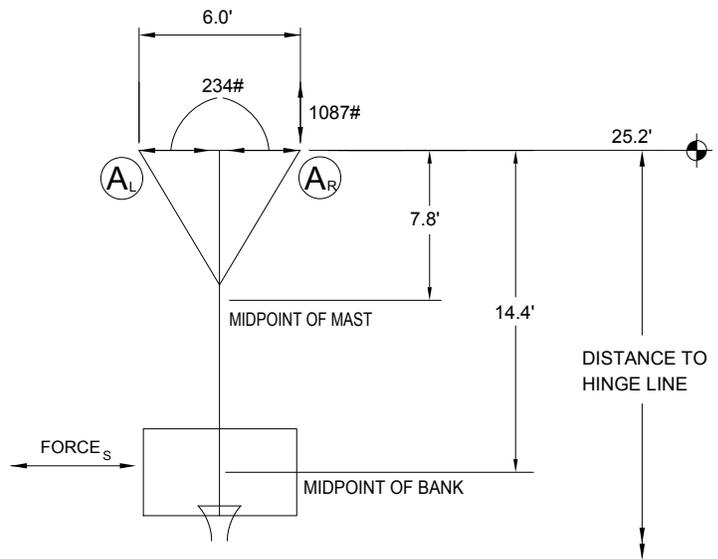
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	trmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	670 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		613 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK	
WEIGHT LOAD AT POINT "B" =		57 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	2667 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	41 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	207 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	329 lbs X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	1806 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 4680 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $1087 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $234 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $502 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $324 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $636 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $17 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A FROM SEISMIC PARALLEL TO BANK: $780 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $692 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $636 \text{ lbs} = \text{HOIST CABLE TENSION}$



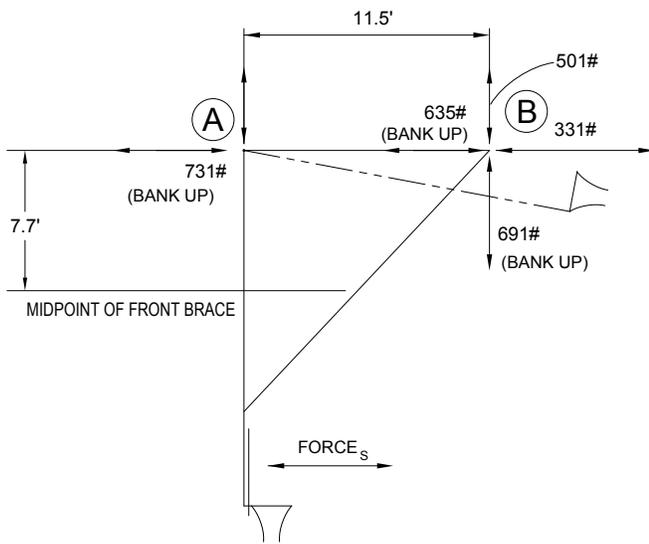
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
26' Attachment Height

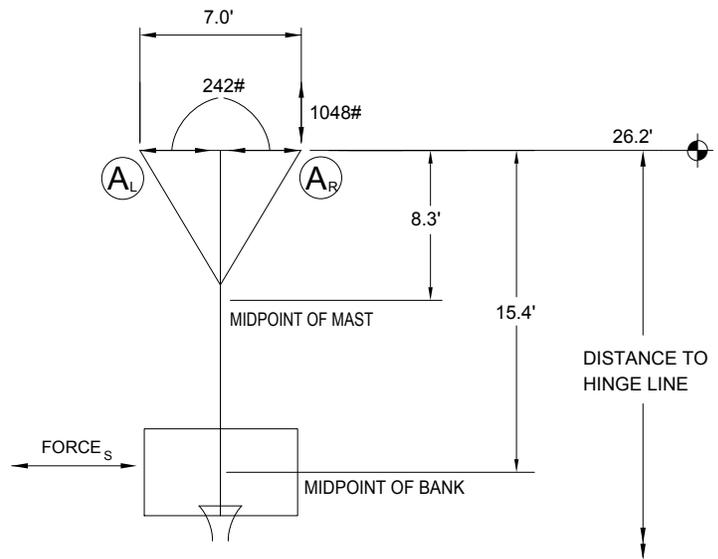
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	691 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		634 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK	
WEIGHT LOAD AT POINT "B" =		57 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	264 lbs	X SEISMIC FACTOR	X	DISTANCE TO MIDPOINT OF BANK (DB)	=	2852 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	41 lbs	X SEISMIC FACTOR	X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	221 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	350 lbs	X SEISMIC FACTOR	X	DISTANCE TO MIDPOINT OF MAST (DM)	=	2042 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 5115 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN	R_{VER}^A	VERTICAL REACTIONS AT POINT A:	1048 lbs =	$\frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$
	R_{HOR}^A	HORIZONTAL REACTION AT POINT A:	242 lbs =	$\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN	R_{VER}^B	VERTICAL REACTION AT POINT B:	501 lbs =	$\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$
	R_{HOR}^B	HORIZONTAL REACTION AT POINT B:	331 lbs =	$\frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: 635 lbs = $\frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{A-BU}	VERTICAL REACTION AT POINT A:	28 lbs =	$\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$
	R_{HOR}^{A-BU}	HORIZONTAL REACTION AT POINT A: FROM SEISMIC PARALLEL TO BANK	731 lbs =	$\pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP	R_{VER}^{B-BU}	VERTICAL REACTION AT POINT B:	691 lbs =	HOIST CABLE TENSION + $\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$
	R_{HOR}^{B-BU}	HORIZONTAL REACTION AT POINT B:	635 lbs =	HOIST CABLE TENSION



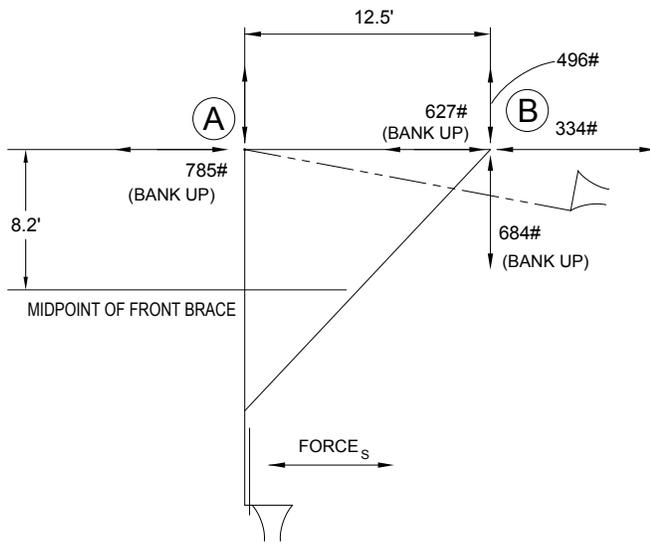
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE	5/9/2011	

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
27' Attachment Height

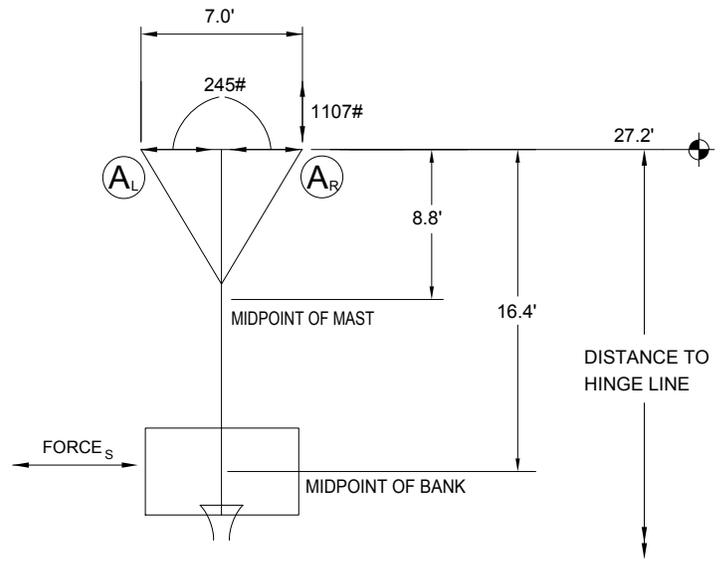
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 700 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = $644 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = $57 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB) 264 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF BANK (DB) = 3037 ft.lbs SEISMIC MOMENT (MB) (FT.LBS.)

WEIGHT OF FRONT BRACE (WFB) 41 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF FRONT BRACE (DFB) = 236 ft.lbs SEISMIC MOMENT (MFB) (FT.LBS.)

WEIGHT OF MAST (WM) 359 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF MAST (DM) = 2222 ft.lbs SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 5494 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $1107 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)_R}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $245 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $496 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $334 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $627 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $36 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $785 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $684 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $627 \text{ lbs} = \text{HOIST CABLE TENSION}$



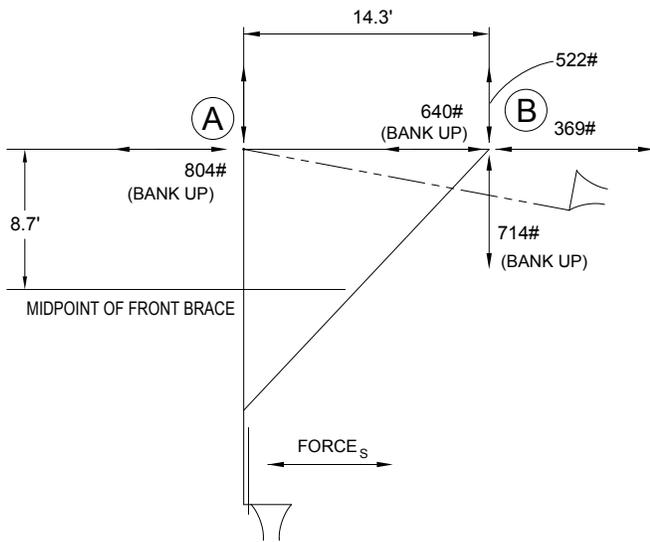
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		
5/9/2011		

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
28' Attachment Height

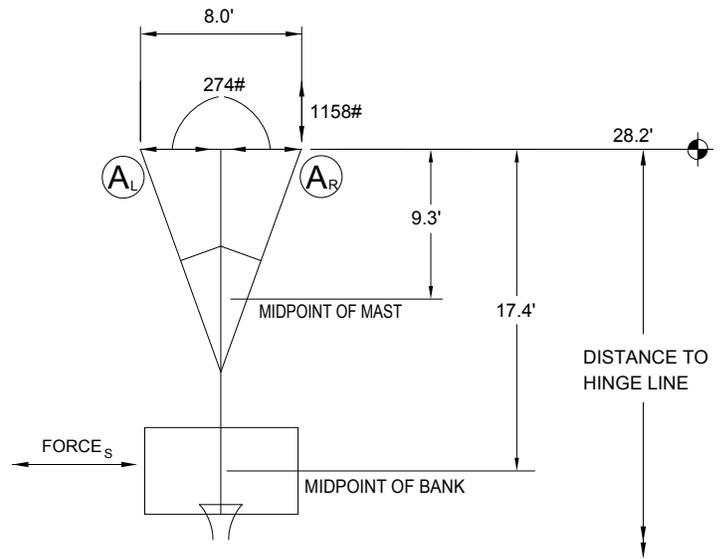
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	trmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 782 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MOST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = $708 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = $74 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB) 280 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF BANK (DB) = 3417 ft.lbs SEISMIC MOMENT (MB) (FT.LBS.)

WEIGHT OF FRONT BRACE (WFB) 76 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF FRONT BRACE (DFB) = 464 ft.lbs SEISMIC MOMENT (MFB) (FT.LBS.)

WEIGHT OF MAST (WM) 390 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF MAST (DM) = 2551 ft.lbs SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 6432 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $1158 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $274 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} \times \text{SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $522 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $369 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE} \times 2}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $640 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR} \times \text{DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $71 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $804 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $714 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $640 \text{ lbs} = \text{HOIST CABLE TENSION}$



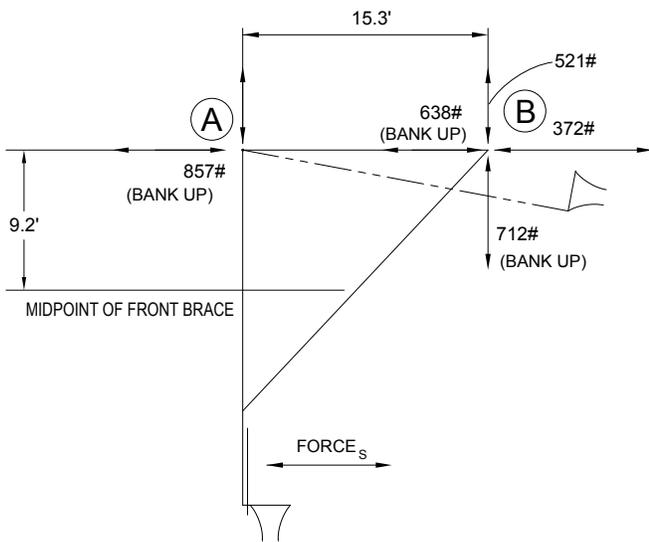
REVISION	DATE	PORTER No. C11
A	6/7/95	
B	7/31/95	CUSTOMER No. 3064
C	6/1/99	
DATE		5/9/2011

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
29' Attachment Height

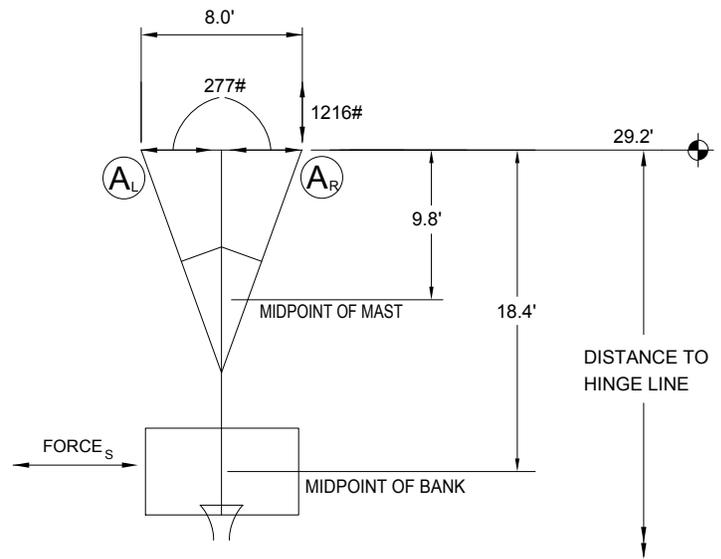
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT
2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	trmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 792 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = 718 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK

WEIGHT LOAD AT POINT "B" = 74 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB) 280 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF BANK (DB) = 3613 ft.lbs SEISMIC MOMENT (MB) (FT.LBS.)

WEIGHT OF FRONT BRACE (WFB) 76 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF FRONT BRACE (DFB) = 490 ft.lbs SEISMIC MOMENT (MFB) (FT.LBS.)

WEIGHT OF MAST (WM) 400 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF MAST (DM) = 2752 ft.lbs SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 6855 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: 1216 lbs = $\frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: 277 lbs = $\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: 521 lbs = $\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: 372 lbs = $\frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: 638 lbs = $\frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: 77 lbs = $\frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: 857 lbs = $\pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L \text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: 712 lbs = HOIST CABLE TENSION + $\frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: 638 lbs = HOIST CABLE TENSION



REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		
5/9/2011		

STATIC EQUIVALENT LOADING FOR:

949 Style Backstop

30' Attachment Height

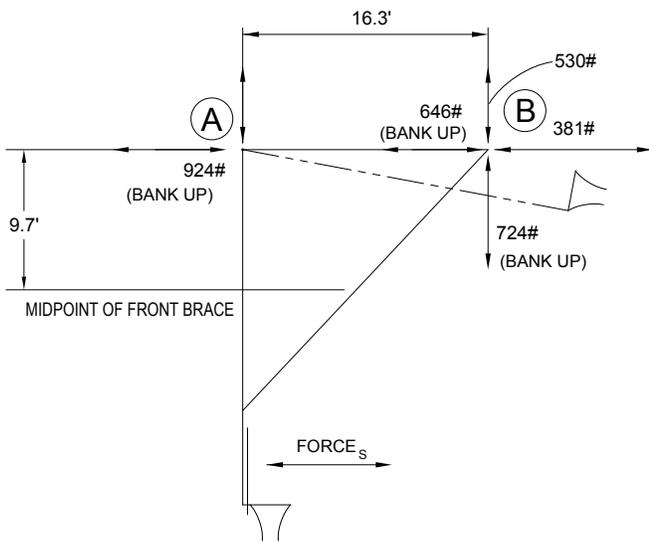
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER

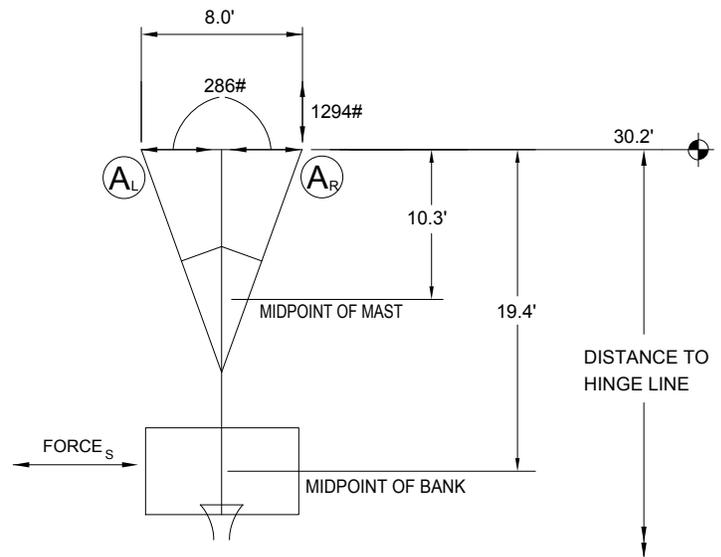
WORLD LEADER
IN QUALITY SPORTS EQUIPMENT

2500 S. 25th AVENUE
BROADVIEW, ILLINOIS 60155
www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD = 817 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK) + PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.

WEIGHT LOAD AT POINT "A" = $739 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF MAST} + \text{WEIGHT OF BANK}$

WEIGHT LOAD AT POINT "B" = $78 \text{ lbs} \left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right) + \text{WEIGHT OF PULLEY}$

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB) 280 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF BANK (DB) = 3809 ft.lbs SEISMIC MOMENT (MB) (FT.LBS.)

WEIGHT OF FRONT BRACE (WFB) 84 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF FRONT BRACE (DFB) = 571 ft.lbs SEISMIC MOMENT (MFB) (FT.LBS.)

WEIGHT OF MAST (WM) 417 lbs X SEISMIC FACTOR X DISTANCE TO MIDPOINT OF MAST (DM) = 3016 ft.lbs SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 7396 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $1294 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS } (A_L - A)_R}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $286 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $530 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS } (A-B)}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $381 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $646 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $85 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $924 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM } A_L \text{ TO } A_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $724 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $646 \text{ lbs} = \text{HOIST CABLE TENSION}$



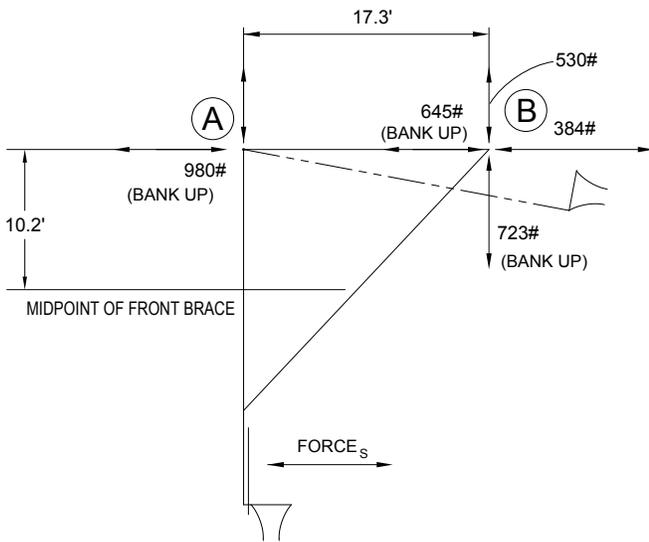
REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE		
5/9/2011		

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
31' Attachment Height

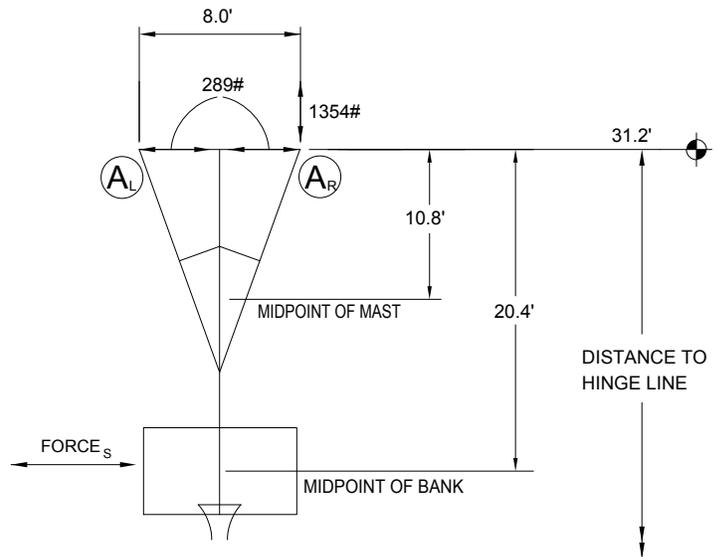
THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

porter
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	



FORCES PERPENDICULAR TO BANK FIGURE 1



FORCES PARALLEL TO BANK FIGURE 2

WEIGHT LOAD CALCULATIONS (WITH BANK DOWN)

BACKSTOP'S TOTAL WEIGHT LOAD	=	826 lbs (WEIGHT OF FRONT BRACE + WEIGHT OF MAST + WEIGHT OF BANK	+ PLEASE NOTE THESE ARE ESTIMATED WEIGHT LOADS FROM THE BACKSTOP MAST HANGERS TO THE FLOOR. THESE ESTIMATES DO NOT INCLUDE ANY SUPERSTRUCTURE WEIGHTS.
WEIGHT LOAD AT POINT "A" =		748 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF MAST + WEIGHT OF BANK	
WEIGHT LOAD AT POINT "B" =		78 lbs $\left(\frac{\text{WEIGHT OF FRONT BRACE}}{2} \right)$ + WEIGHT OF PULLEY	

SEISMIC FACTORED MOMENTS AND SUM OF MOMENTS FOR BACKSTOP ELEMENTS

SEISMIC FACTOR = 0.7 (VARIES WITH SEISMIC ZONE, RIGIDITY OF SUPPORT & ROOM USE)

WEIGHT OF BANK (WB)	280 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF BANK (DB)	=	4005 ft.lbs	SEISMIC MOMENT (MB) (FT.LBS.)
WEIGHT OF FRONT BRACE (WFB)	84 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF FRONT BRACE (DFB)	=	601 ft.lbs	SEISMIC MOMENT (MFB) (FT.LBS.)
WEIGHT OF MAST (WM)	426 lbs	X SEISMIC FACTOR X	DISTANCE TO MIDPOINT OF MAST (DM)	=	3232 ft.lbs	SEISMIC MOMENT (MM) (FT.LBS.)

WB + WFB + WM = BACKSTOP'S TOTAL WEIGHT LOAD = 7838 ft.lbs SUM OF THE MOMENTS = MB + MFB + MM

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK DOWN

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK DOWN

R_{VER}^A VERTICAL REACTIONS AT POINT A: $1354 \text{ lbs} = \frac{\text{WEIGHT LOAD AT POINT "A"}}{2 \text{ SUPPORTS}} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A}_L\text{A}_R)}$

R_{HOR}^A HORIZONTAL REACTION AT POINT A: $289 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD X SEISMIC FACTOR}}{2 \text{ SUPPORTS}}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PERPENDICULAR TO BANK (FIG. 1)

BANK DOWN

R_{VER}^B VERTICAL REACTION AT POINT B: $530 \text{ lbs} = \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY} \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE BETWEEN SUPPORTS (A-B)}}$

R_{HOR}^B HORIZONTAL REACTION AT POINT B: $384 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE TO MIDPOINT OF FRONT BRACE X 2}}$

POINT REACTIONS FROM WEIGHT LOADS AND SEISMIC WITH BANK UP

HOIST CABLE TENSION AT POINT C: $645 \text{ lbs} = \frac{\text{SUM OF THE MOMENTS}}{\text{SEISMIC FACTOR X DISTANCE FROM A TO B}}$

REACTIONS AT HINGE LINE AT POINT A FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{A-BU} VERTICAL REACTION AT POINT A: $90 \text{ lbs} = \frac{\text{BACKSTOP'S TOTAL WEIGHT LOAD} - \text{HOIST CABLE TENSION}}{2 \text{ SUPPORTS}}$

R_{HOR}^{A-BU} HORIZONTAL REACTION AT POINT A: $980 \text{ lbs} = \pm \frac{\text{SUM OF THE MOMENTS}}{\text{DISTANCE FROM A}_L\text{ TO A}_R}$

REACTIONS AT HINGE LINE AT POINT B FROM WEIGHT LOADS AND SEISMIC PARALLEL TO BANK (FIG. 2)

BANK UP

R_{VER}^{B-BU} VERTICAL REACTION AT POINT B: $723 \text{ lbs} = \text{HOIST CABLE TENSION} + \frac{\text{WEIGHT OF FRONT BRACE}}{2 \text{ SUPPORTS}} + \text{WEIGHT OF PULLEY}$

R_{HOR}^{B-BU} HORIZONTAL REACTION AT POINT B: $645 \text{ lbs} = \text{HOIST CABLE TENSION}$



REVISION	DATE	PORTER No.
A	6/7/95	C11
B	7/31/95	CUSTOMER No.
C	6/1/99	3064
DATE	5/9/2011	

STATIC EQUIVALENT LOADING FOR:
949 Style Backstop
32' Attachment Height

THIS PRINT IS THE PROPERTY OF PORTER ATHLETIC EQUIPMENT COMPANY AND MAY NOT BE REPRODUCED WITHOUT WRITTEN PERMISSION

PORTER
 WORLD LEADER
 IN QUALITY SPORTS EQUIPMENT
 2500 S. 25th AVENUE
 BROADVIEW, ILLINOIS 60155
 www.porter-ath.com

DRAWING BY	tmathis
CHECKED BY	GS
PAGE No.	